

*System And Method Of Operation Of An Array Antenna In A
Distributed Wireless Communication Network*

Cross-Reference to Related Application

5 This application claims priority from United States Provisional Patent Application Serial No. 60/453,840, filed on March 11, 2003. The entire contents of this provisional application are hereby incorporated herein by reference.

10 This application is also related to the following Provisional Patent Applications filed in the U.S. Patent and Trademark Office, the disclosures of which are expressly incorporated herein by reference:

- 15 • U.S. Patent Application Serial No. 60/446,617 filed on Feb. 11, 2003 and entitled "System for Coordination of Multi Beam Transit Radio Links for a Distributed Wireless Access System" [15741]
- 20 • U.S. Patent Application Serial No. 60/446,618 filed on Feb. 11, 2003 and entitled "Rendezvous Coordination of Beamed Transit Radio Links for a Distributed Multi-Hop Wireless Access System" [15743]
- 25 • U.S. Patent Application Serial No. 60/446,619 filed on Feb. 12, 2003 and entitled "Distributed Multi-Beam Wireless System Capable of Node Discovery, Rediscovery and Interference Mitigation" [15742]
- U.S. Patent Application Serial No. 60/447,527 filed on Feb. 14, 2003 and entitled "Cylindrical Multibeam Planar Antenna Structure and Method of Fabrication" [15907]

- U.S. Patent Application Serial No. 60/447,643 filed on Feb. 14, 2003 and entitled "An Omni-Directional Antenna" [15908]
- U.S. Patent Application Serial No. 60/447,644 filed on Feb. 14, 2003 and entitled "Antenna Diversity" [15913]
- U.S. Patent Application Serial No. 60/447,645 filed on Feb. 14, 2003 and entitled "Wireless Antennas, Networks, Methods, Software, and Services" [15912]
- U.S. Patent Application Serial No. 60/447,646 filed on Feb. 14, 2003 and entitled "Wireless Communication" [15897]
- U.S. Patent Application Serial No. 60/451,897 filed on March 4, 2003 and entitled "Offsetting Patch Antennas on an Omni-Directional Multi-Faceted Array to allow Space for an Interconnection Board" [15958]
- U.S. Patent Application Serial No. 60/453,011 filed on March 7, 2003 and entitled "Method to Enhance Link Range in a Distributed Multi-hop Wireless Network using Self-Configurable Antenna" [15946]
- U.S. Patent Application Serial No. 60/ 454,715 filed on March 15, 2003 and entitled "Directive Antenna System in a Distributed Wireless Network" [15952]
- U.S. Patent Application Serial No. 60/461,344 filed on April 9, 2003 and entitled "Method of Assessing Indoor-Outdoor Location of Wireless Access Node" [15953]
- U.S. Patent Application Serial No. 60/461,579 filed on April 9, 2003 and entitled "Minimisation of Radio Resource

Usage in Multi-Hop Networks with Multiple Routings"
[15930]

- U.S. Patent Application Serial No. 60/464,844 filed on
April 23, 2003 and entitled "Improving IP QoS through Host-
5 Based Constrained Routing in Mobile Environments" [15807]
- U.S. Patent Application Serial No. 60/467,432 filed on May
2, 2003 and entitled "A Method for Path Discovery and
Selection in Ad Hoc Wireless Networks" [15951]
- U.S. Patent Application Serial No. 60/468,456 filed on May
10 7, 2003 and entitled "A Method for the Self-Selection of
Radio Frequency Channels to Reduce Co-Channel and Adjacent
Channel Interference in a Wireless Distributed Network"
[16101]
- U.S. Patent Application Serial No. 60/480,599 filed on
15 June 20, 2003 and entitled "Channel Selection" [16146]

Field of the Invention

This invention relates generally to array
antennas, and, in particular, to the operation of such
antennas.

20 Background of the Invention

In wireless communication networks, the capacities
of wireless communication links between network nodes are
dependent upon received signal power relative to noise and
interference, often expressed as a signal to noise and
25 interference ratio or SNIR. Received signal power is
affected by such link characteristics as link length and
physical obstructions or "shadowing".

Directional antennas are commonly used to mitigate the effects of shadowing. However, antennas are often deployed in constrained locations such as on street lights, utility poles, and the like, and are therefore limited in size. Size limitations in turn limit the directionality of these antennas, which thereby renders the antennas more susceptible to interference.

Although conventional high gain directional antennas may increase received signal power, known manual alignment techniques by which such antennas are aligned with existing network nodes are labor intensive. For example, when a network node is added to a communication network, a new antenna may need to be added to and aligned at each existing network node with which the new network node is to communicate. Alternatively, a high gain antenna need not necessarily be implemented at both ends of each transit link between network nodes, but such transit links then do not fully derive the benefits of high gain directional antennas.

Further, high gain directional antennas, by their nature, are characterized by narrow radiation and reception patterns or beams. Beamwidth generally decreases with increasing gain. Whereas highly directional beams may improve SNIR and increase wireless link capacity, scan times to detect incoming communication signals from neighbouring network nodes tend to increase, particularly for network nodes that communicate with multiple other network nodes. For these nodes, a greater number of antennas are required to cover a full 360 degrees, and each antenna is typically scanned to detect incoming communications.

Summary of the Invention

A system for operating an array antenna having multiple antenna elements is provided in accordance with one aspect of the invention. The system includes a feeding port, signal shifters, and an adaptive beamformer. The
5 signal shifters are connected to respective antenna elements. The adaptive beamformer distributes input signals from the feeding port to the signal shifters and combines output signals from the signal shifters for output to the feeding port in different operating modes. Each operating
10 mode is associated with respective array antenna gain patterns having different beamwidths.

According to another aspect of the invention, a network node for a distributed wireless access network includes a steerable array antenna having multiple antenna
15 elements and configurable beamwidth for establishing wireless transit radio links with neighbouring network nodes in the distributed wireless access network, signal shifters for respective connection to the antenna elements, and an adaptive beamformer. The adaptive beamformer distributes
20 array antenna input signals to the signal shifters and combines array antenna output signals from the signal shifters in a wide beamwidth operating mode associated with an array antenna gain pattern having a first beamwidth and a narrow beamwidth operating mode associated with an array
25 antenna gain pattern having a second beamwidth narrower than the first beamwidth.

In one embodiment, the adaptive beamformer includes multiple beamformers that distribute input signals from the feeding port to, and combine output signals from,
30 particular ones of the signal shifters.

The signal shifters may be phase shifters or combined amplitude and phase shifters. For phase shifters, phase weights to steer a gain pattern of the array antenna in particular directions, toward network nodes in a distributed wireless access network, for example, are determined. In embodiments including combined phase and amplitude shifters, complex weights having both phase components and amplitude components to steer gain peaks and nulls in an array antenna gain pattern are determined.

10 In accordance with another aspect of the invention, a method of operating an array antenna having configurable beamwidth in a wireless communication network is provided. The method includes listening for communication requests using a first beamwidth of the array antenna, receiving a communication request identifying a destination wireless access routing point in the wireless communication network, forming a beam having a second beamwidth narrower than the first beamwidth, directing the formed beam toward the destination wireless access routing point, and transmitting communication signals over the formed beam to the destination wireless access routing point.

25 In a particular embodiment of the method, directing involves accessing a lookup table to retrieve phase shifts for antenna elements in the array antenna to steer the formed beam toward the destination wireless access routing point and applying the phase shifts to respective excitation signals of the antenna elements.

30 Another embodiment of the method includes determining a location of an interferer and directing a null toward the interferer. Directing a null toward the

interferer may be accomplished by calculating phase and amplitude shifts for antenna elements in the array antenna to steer the null toward the interferer and applying the phase and amplitude shifts to respective excitation signals
5 of the antenna elements.

According to yet another aspect of the invention, a system for operating an array antenna element in a wireless communication network is provided. The array antenna is excited to form a beam having a first beamwidth
10 to listen for communication requests. After a communication request identifying a destination wireless access routing point in the wireless communication network is received, the array antenna is excited to form a beam having a second beamwidth narrower than the first beamwidth, and the formed
15 beam is directed toward the destination wireless access routing point. Communication signals are then transmitted to the destination wireless access routing point over the beam having the second beamwidth.

A distributed wireless access network, in
20 accordance with a still further aspect of the invention, includes network access nodes and wireless transit radio links between the network access nodes. At least one of the network access nodes has an electronically steerable high gain array antenna with configurable beamwidth for
25 establishing wireless transit links with its neighbouring network access nodes.

Operation of an antenna system at such different beamwidths enables the benefits of both wide antenna beams and directional antenna beams to be realized. For example,
30 wide antenna beams reduce scan times for detecting incoming communication signals, whereas narrow directional antenna

beams generally have higher gains and may be preferred for communication signal transmission. Beam and null steering in accordance with some embodiments of the invention further reduce interference on wireless communication links.

5 Other aspects and features of the present invention will become apparent to those ordinarily skilled in the art upon review of the following description of the specific embodiments of the invention.

Brief Description of the Drawings

The invention will now be described in greater detail with reference to the accompanying diagrams, in which:

5 Fig. 1 is a block diagram of a distributed wireless communication network;

 Fig. 2 is a block diagram of a wireless access routing point of Fig. 1;

10 Fig. 3 is a line drawing illustrating beam steering in a linear array antenna;

 Fig. 4 is a block diagram of a patch array antenna and associated feed arrangement;

 Fig. 5 is a plot of an example array antenna gain pattern for uniform antenna element excitation;

15 Fig. 6 is a plot of an example array antenna gain pattern for a nonuniform antenna element excitation;

 Fig. 7 is a block diagram of an array antenna feed arrangement according to an embodiment of the invention; and

20 Figs. 8-12 are plots of example array antenna gain patterns for excitation of different numbers of antenna elements.

Detailed Description of Preferred Embodiments

25 Fig. 1 is a block diagram of a distributed wireless communication network, in which the present invention may be implemented. The wireless communication

network comprises a network access point (NAP) 10, connected to a wired network via a connection 12, a plurality of wireless access routing points (WARPs) 14, 16, 18, 20, 22, and 24, and a plurality of wireless transit links 26, 28, 5 30, 31, 32, 34, 36, 38, and 40. The network shown in Fig. 1 is one example of the type of communication network to which the present invention is applicable. The invention is in no way restricted to the network of Fig. 1, and may be implemented in other types of networks having different 10 numbers and types of network nodes, including networks without a NAP or other connection to a wired network, for instance.

As shown, the NAP 10 is a network node that is connected to a wired backbone network such as the Internet 15 through the connection 12, typically a broadband wireline connection.

The WARPs 14, 16, 18, 20, 22, and 24 route communication signals throughout the network, and possibly outside the network through the NAP 10, via transit links 20 26, 28, 30, 31, 32, 34, 36, 38, and 40. Although not explicitly shown in Fig. 1, those skilled in the art will appreciate that the WARPs also support a network access function allowing mobile stations to access the network.

Any of the WARPs 14, 16, 18, 20, 22, and 24 that 25 require connection outside the local network shown in Fig. 1 must establish a connection through the NAP 10. As such, the capacity of the wireless transit links 26 and 28 is of critical importance and, in some instances, may represent a bottleneck in the network. Although antenna operation as 30 described herein is particularly pertinent to such critical

wireless links, it should be appreciated that the invention is in no way limited thereto.

As described above, the capacity of a wireless link is dependent upon its SNIR. In accordance with an aspect of the present invention described in further detail below, an adaptive array antenna is operated in one of a plurality of operating modes, including a wide beam scanning mode and a high gain directional operating mode that supports high capacity wireless links.

Fig. 2 is a block diagram of a wireless access routing point of Fig. 1. Each of the WARPs 16, 18, 20, 22, and 24 preferably has a similar structure to the WARP 14 shown in Fig. 2.

The WARP 14 comprises an access radio 48 connected to an access antenna 49, a communications controller 46 connected to the access radio 48, a weight calculator 50, and a transit radio 44, and a steered array antenna 52 connected to the transit radio 44 and the weight calculator 50. A WARP may also include further components that have not been shown in Fig. 2 to avoid congestion in the drawing.

The access radio 48 and the antenna 49 support a network access function for mobile stations (not shown) located within an access coverage area of the WARP 14. The access radio 48 performs such operations as communication signal frequency conversion, filtering, encoding and decoding, and modulation and demodulation, for example. The antenna 49 transmits communication signals to and receives communication signals from mobile stations, and comprises either a single antenna element or multiple antenna elements such as main and diversity antenna elements.

The operation of the communications controller 46 is dependent upon the design and configuration of the WARP 14. Generally, a communications controller handles such control functions as routing of communication signals
5 between the transit radio 44 and the access radio 48 and control of scanning operations by the transit radio 44 and the access radio 48.

The transit radio 44 performs operations similar to those of the access radio 48, to support transit links to
10 one or more other WARPs. However, the access radio 48 and the transit radio 44 typically employ different frequency bands, and possibly different encoding and modulation schemes. For example, in one embodiment, the access radio 48 is an 802.11b/g module operating at 2.4GHz, whereas the
15 transit radio 44 is an 802.11a module operating in the frequency band of 5.15GHz to 5.85GHz. Those skilled in the art will appreciate that "802.11" refers to a set of specifications, available from the Institute of Electrical and Electronics Engineers (IEEE) relating to wireless local
20 area networks (LANs).

The steered array antenna 52 transmits and receives communication signals over the wireless transit links 26, 31, and 32. The array antenna 52 includes a plurality of antenna elements. Gain patterns of the
25 individual antenna elements interfere both constructively and destructively to generate a resultant gain pattern of the array antenna 52. Beamwidth and direction of the resultant gain pattern are controllable, as described in further detail below, by applying phase weights to
30 excitation signals of each antenna element.

Fig. 3 is a line drawing illustrating beam steering in a linear array antenna. As shown, beams 72, 74, 76, and 78 from each antenna element 62, 64, 66, and 68 in a linear array antenna are steered in a beam pointing direction θ relative to boresight, indicated at 70. Beam steering is achieved by phase shifting antenna feed or excitation signals, which include both received and transmitted signals. Progressive phase shifts ϕ_n between antenna elements in an array antenna are calculated, by the weight calculator 50 in Fig. 2, for example, according to the following formula:

$$\phi_n = n * (2\pi/\lambda)d * \sin\theta,$$

where $n = 0, 1, \dots, n$ for an array antenna having $n + 1$ elements, λ is wavelength associated with an operating frequency of the array antenna, and d is the spacing between antenna elements. Where an array antenna is operable within a range of frequencies, λ is preferably the minimum wavelength λ_{min} associated with the maximum operating frequency. For the four-element array antenna shown in Fig. 3, the phase weights for the antenna elements 62, 64, 66, and 68 are $0, (2\pi/\lambda)d * \sin\theta, (4\pi/\lambda)d * \sin\theta,$ and $(6\pi/\lambda)d * \sin\theta,$ respectively.

For any distance d between antenna elements, there is a maximum useful beam steering angle θ_{max} . For beam pointing angles beyond the maximum steering angle, so-called grating lobes appear in the antenna gain pattern. However, grating lobes can be reduced by establishing the distance d as follows:

$$d \leq \lambda_{min}/(1 + \sin|\theta_{max}|).$$

In a preferred embodiment of the invention, the transit radio 44 (Fig. 2) is an 802.11a module with a maximum operating frequency of 5.85GHz. For a +/-60 degree beam scan (i.e., $|\theta_{max}| = 60$ degrees), antenna element spacing is approximately 27mm. This antenna element spacing restricts the type of antenna elements that may be used, in that the antenna elements must be relatively small in the horizontal plane. Vertically polarized dipole antennas represent one example of a type of antenna element that can be used to realize such an array antenna. With a +/- 60 degree beam scan, three such array antennas arranged in a triangle cover a full 360 degrees. A reduced scan range of +/- 45 degrees allows for a larger antenna element spacing and thus an easier to achieve design, but requires four array antennas instead of three to cover 360 degrees. Of course, other beam scan ranges can also be used.

Another alternative antenna element structure is a patch antenna. Fig. 4 is a block diagram of a patch array antenna and associated feed arrangement.

The patch array antenna 80 includes a plurality of radiating elements 82 arranged in 4 rows and $n + 1$ columns. The feed arrangement includes a feeding port 94, a beamformer 92, and one phase shifter 84, 86, 88, and 90 per column.

Phase shifters are commercially available and are typically characterized by a number of control bits. For example, a 6-bit phase shifter has phase steps of $360/2^6$, or 5.625 degrees. The phase shifters 84, 86, 88, and 90 are selected to ensure that the quantization phase steps are sufficiently small to provide desired antenna beamwidth and pointing accuracy. The phase shifts applied by the phase

shifters 84, 86, 88, and 90 are controlled by phase weights calculated and supplied by a weight calculator such as the weight calculator 50 of Fig. 2.

During a transmit operation, the beamformer 92 distributes an excitation signal received on the feeding port 94 to the phase shifters 84, 86, 88, and 90. In a similar manner, the beamformer 92 combines signals received from the phase shifters 84, 86, 88, and 90 and provides output signals on the feeding port 94.

Several design options for the beamformer 92 will be apparent to those skilled in the art. In perhaps its simplest implementation, the beamformer 92 is an equal power divider/combiner, providing the highest possible gain. Fig. 5 is a plot of an example array antenna gain pattern for such a uniform antenna element excitation. Although uniform excitation typically provides highest possible gain, sidelobe levels are approximately 13dB below the peak gain. In some embodiments, the beamformer 92 can be configured to apply an amplitude taper across the array antenna 80 to reduce sidelobe levels and thus provide increased immunity to interference, albeit at the expense of slightly reduced peak gain. Fig. 6 is a plot of an example array antenna gain pattern for a nonuniform antenna element excitation that achieves sidelobe levels at 30dB below peak gain. Further alternative beamformers will be apparent to those skilled in the art to which the present invention pertains.

For a patch array antenna, maximum achievable gain is typically determined as:

$$G = 4\pi A_{eff}/\lambda^2,$$

Where A_{eff} = effective area of the patch array antenna.

As an example, consider a patch array antenna operated at a centre frequency of 5.4GHz and wherein elements are arranged in four rows spaced at $.75\lambda$ with 36 columns spaced 27mm apart to allow +/- 60 degree scanning.

5 $A_{eff} = \text{height} * \text{width} = (4*42)*(36*27) = 168\text{mm}*972\text{mm} = 0.16\text{m}^2$.
With an assumed efficiency of 50%, actual gain is approximately 25.2dBi, which represents a link budget gain of over 10dB relative to typical gains of about 14dBi for
10 array antennas can thereby either be operated at greater range or significantly higher data rates.

A patch array antenna may also be implemented, for example, with dielectrically loaded dual polarized patch antenna elements. In this configuration, dielectric loading
15 reduces the size of the patch for resonance, thereby enabling smaller element spacing and reducing grating lobes. Dual polarized patches also provide for such further benefits as individual beam steering, polarization diversity for both transmit and receive operations, and implementation
20 of multiple input multiple output (MIMO). In a dual polarized array antenna, a feeding port, a beamformer, and a plurality of phase shifters are preferably provided for each of vertical and horizontal polarizations or other orthogonal polarizations.

25 Fig. 7 is a block diagram of an array antenna feed arrangement according to an embodiment of the invention. The feed arrangement includes a phase shifter 102, 104, 106, 108, 110, and 112 for each antenna element in the array antenna, or for each column of antenna elements in a patch
30 array antenna, a plurality of switches 114 and 116, a plurality of beamformers 118 and 120, an input/output switch 122, and a feeding port 124. The beamformers 118 and 120

and the switches 114, 116, and 122 represent one implementation of an adaptive beamformer which, as described in further detail below, distributes input signals from the feeding port 124 to the phase shifters 102-112 and combines
5 output signals from the phase shifters 102-112 for output to the feeding port 124. In alternate embodiments, the adaptive beamformer and the phase shifters 102-112 are implemented digitally, with frequency upconverting for signals to be transmitted and frequency downconverting for
10 received signals.

The phase shifters 102-112 operate substantially as described above, applying phase shifts dependent upon phase weights received from a weight calculator.

In Fig. 7, both of the beamformers 118 and 120 are
15 configured to process signals for the centre two phase shifters 108 and 110 and their associated antenna elements, but only one beamformer, 120, is configured to process signals for the remaining phase shifters and associated antenna elements. The switches 114 and 116 provide for
20 selection of either the beamformer 118 or the beamformer 120. Similarly, the input switch 122 routes an input signal to or an output signal from a selected one of the beamformers 118 and 120.

As described above, high gain directional antennas
25 are desirable for increasing signal power and reducing interference, but can increase scan times for detecting incoming connection or link requests from a neighbouring WARPs. In the system of Fig. 7, the beamformers 118 and 120 provide for different operating modes of an array antenna.
30 During a scan operation, a wide beamwidth operating mode is selected, whereas during communication operations in which

communication signals are being transmitted or received, a more directional narrow beamwidth operating mode is preferably selected. Beamwidth effects of different array antenna excitations will become apparent from the following description and Figs. 8-12, which are plots of array antenna gain patterns for excitation of different numbers of antenna elements. The plots in Figs. 8-12 represent gain patterns for the above example 4 row by 36 column patch array antenna.

As shown in Fig. 8, selection of the beamformer 118, associated with excitation of only the centre two antenna elements in an array antenna, results in a relatively large beamwidth of 62 degrees. In this example, a full 360 degree scan is achieved with three array antennas. This wide beamwidth is used, for example, in a scanning mode to await the arrival of a transit link request from a neighbouring WARP, thereby reducing scan times relative to known directional antenna implementations, or in other situations in which a wide beamwidth is desirable.

For communication operations, a more directional antenna pattern is generally preferred to increase received signal power and reduce interference. When a transit link request from a neighbouring WARP or a communication signal from a mobile station within an access area of a WARP is received, for example, a high gain directional operating mode is preferably selected. For a transit link request, an identifier of the requesting WARP is decoded from the request, and a previously generated lookup table or other mapping means from which the phase weights associated with steering a beam toward neighbouring WARPs can be retrieved or determined is accessed. Phase weights for neighbouring WARPs may be manually determined and stored, for example,

when a WARP is installed in a network. In another embodiment, a WARP is configured to discover its neighbouring WARPs to populate a lookup table. Discovery techniques are disclosed, for example, in the co-pending and
5 commonly assigned United States Patent Application Serial No. <Attorney Docket No. 71493-1196>, entitled "Distributed Multi-Beam Wireless System", and filed of even date herewith, the entire contents of which are hereby
10 determining a location of a neighbouring WARP may also be apparent to those skilled in the art, and as such are considered to be within the scope of the present invention.

The phase weights required to steer the antenna pattern in the direction of the neighbouring WARP are
15 retrieved from the lookup table and applied to the phase shifters 102-112. The beamformer 120 is selected, and the switches 122, 114, and 116 are set accordingly. As shown in Fig. 12, excitation of all 36 antenna elements results in a much narrower beamwidth of 4 degrees, steered in the
20 direction of the appropriate neighbouring WARP. The high gain and low interference enables high data rate communications over the wireless link.

Thus, an array antenna operated in this manner has configurable beamwidth. A wide beamwidth operating mode is
25 useful for such functions as scanning or listening for incoming communication traffic or link requests. The high gain directional or narrow beamwidth operating mode for communication functions simultaneously increases received signal power and reduces interference. Both operating modes
30 are provided using a single antenna structure and phase shifters.

Beamformer selection, switch control, and thus radiation pattern selection, are preferably performed by a communications controller, a transit radio, or some other WARP component dependent upon a current or desired operating
5 mode.

In further embodiments, operating modes use other than the two centre antenna elements and all of the antenna elements indicated in Fig. 7. Figs. 9-11 illustrate array antenna gain patterns associated with using 4, 10, and 20
10 antenna elements, respectively, of the same patch array antenna for which the plots of Figs. 8 and 12 were generated.

In another embodiment, further intermediate beamformers are provided in an array antenna feeding system.
15 In such systems, more than two operating modes are supported. For instance, it is known that in distributed wireless access networks, links that are not line-of-sight may have many reflections, and many propagation paths exist between a transmitting network node and a receiving network
20 node. If too narrow a beamwidth is selected for such a link, then some of the paths are not excited, and hence additional losses may occur. Accordingly, where several narrow beamwidth beamformers are provided, the beamformer that provides the best link gain available can be selected.
25 Selection of a beamformer is then dependent upon the propagation characteristics of a link between particular WARPs at the time of use. In one possible implementation, current propagation characteristics are determined and a beamformer is selected, or a different beamformer is
30 selected, based on those characteristics. Previous beamformer selections for a particular neighbour WARP may also be recorded, in the lookup table described above, for

example, and used in subsequent communications involving that WARP.

In a still further embodiment, a software-based beamformer module is provided. The beamformer module
5 selects one of a plurality of beamforming algorithms depending upon a current operating mode, provides outputs to or accepts inputs from particular phase shifters as appropriate, and thus does not require the switches 114, 116, and 122. The functionality of the phase shifters 102-
10 112 may also be integrated into such a beamformer module.

The array antenna operation techniques described above use a wide beamwidth for scanning or listening, to locate a source of incoming communication traffic, and a narrow beamwidth for sending or receiving traffic. A wide
15 beam locates a source, and then antenna gain is effectively steered towards the source or to a destination for transmission operations. According to a further aspect of the invention, nulls are placed in an antenna pattern in the direction of interferers, to thereby reduce interference.

20 Antenna gain in an array antenna is steered using phase shifts between antenna elements, as described above. Nulls are also steerable, but using amplitude shifts or offsets in addition to phase shifts. In the case of an interferer having a fixed location relative to a WARP, after
25 the location of the interferer has been determined, either manually or using the wide beamwidth operating mode for instance, complex weights including phase weights and amplitude weights are calculated. The amplitude weights are applied to excitation signals in the beamformers or in
30 separate amplitude shifters or amplifiers, for example. The complex weights for such fixed interferer nulls, like WARP

phase weights, can be stored and retrieved for use in subsequent communication operations.

The wide beamwidth operating mode described above may also be used to locate transient interferers. Transient
5 interferers include interference sources that have no fixed location, a bursty or otherwise discontinuous signalling pattern, or both. Provided the location of such an interferer is determined during a wide beamwidth operating mode, complex weights can be applied to generate a null in
10 the direction of the interferer. Weights associated with such transient interferers may or may not be stored, depending upon system configuration and/or system owner or designer preferences.

Although gain steering and null steering are
15 substantially independent in that each involves a different set of weights, both techniques may be implemented in conjunction with the same antenna. In this instance, phase weights for beam steering and complex weights for null steering are independently calculated and applied to antenna
20 excitation signals as described above. In a preferred embodiment, the phase weights and complex weights are combined after calculation and then applied to excitation signals.

Antenna operation techniques in accordance with
25 aspects of the present invention provide the advantages of high gain and narrow beamwidth during communication operations, while avoiding the scanning or listening time delays associated with conventional high gain antennas. High gain and narrow beamwidth allow longer link ranges to
30 be achieved without interfering with other nodes in a distributed communication network. As such, network routers

such as the WARPs described above are able to direct network traffic to nodes that may otherwise be more than one "hop" away. Multi-hop routing thereby becomes more practical.

Where nodes of a distributed network are located
5 in close proximity and form a dense cluster, power control is often used to reduce the transmitted power to avoid interference between nodes. Operation of an antenna in a high gain and narrow beamwidth mode both maintains the link budget of each wireless link associated with the nodes in
10 the cluster and provides increased immunity to interference between the nodes during communication operations.

What has been described is merely illustrative of the application of the principles of the invention. Other arrangements and methods can be implemented by those skilled
15 in the art without departing from the spirit and scope of the present invention.

For example, although reference is made to a phase weight lookup table stored at a WARP for its neighbouring WARPs, bearing angles may also or instead be stored and
20 retrieved from such a lookup table, and used to calculate appropriate phase weights when a communication link is to be established between WARPs.

In addition, antenna operation systems and methods have been described primarily in the context of network
25 nodes that provide both access and transit functions. However, it should be appreciated that the present invention is applicable to wireless links in general. A network node need not necessarily support access functions.